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### Abstract

Topology optimized SOI mode order converters are proposed to allow mutual conversion between TE<sub>0</sub>, TE<sub>1</sub> and TE<sub>2</sub>. Broadband conversion efficiency around 85% can be realized on an ultra-compact ( 4 micrometer length) footprint.

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# Broadband SOI mode order converter based on topology optimization

Min Teng<sup>1,2</sup>, Keisuke Kojima<sup>1\*</sup>, Toshiaki Koike-Akino<sup>1</sup>, Bingnan Wang<sup>1</sup>,  
Chungwei Lin<sup>1</sup>, and Kieran Parsons<sup>1</sup>

<sup>1</sup>Mitsubishi Electric Research Laboratories, 201 Broadway, Cambridge, MA 02139, USA

<sup>2</sup>School of Electrical and Computer Engineering and the Birck Nanotechnology Center, Purdue University,  
West Lafayette, IN 47907, USA

kojima@merl.com

**Abstract:** Topology optimized SOI mode order converters are proposed to allow mutual conversion between TE<sub>0</sub>, TE<sub>1</sub> and TE<sub>2</sub>. Broadband conversion efficiency around 85% can be realized on an ultra-compact (~ 4 μm length) footprint.

**OCIS codes:** (130.3120) Integrated optics devices; (230.1150) All-optical devices

## 1. Introduction

On-chip mode division multiplexing (MDM) has been heavily researched over decades, which transmits multiple channels in one shared multimode bus waveguide to enhance transmission capacity. A number of MDM devices have been developed, including multiplexers/demultiplexers (MUX/DEMUX), mode order filters and mode order converters. One major challenge of on-chip MDM is the high order mode processing, such as bending and crossing. As a consequence, mode order converters are usually developed to convert high order modes to fundamental mode (TE<sub>0</sub>) first before processing.

Silicon-on-insular (SOI) mode order converters have been proposed by a number of researchers already. The most intuitive converter is to evenly split a high order mode into multiple TE<sub>0</sub> pieces, then merged with proper phase relationship. Recently researchers also numerically proved the mode order converter concept with ultra-low loss based on adiabatic taper on a 30 μm-long footprint [1]. In addition, TE<sub>0</sub>-to-TE<sub>1</sub> converter with more compact footprint (~ 6 μm length) has also been experimentally demonstrated using inverse design [2]. The reported device is optimized inside a photonic crystal waveguide, giving 70% TE<sub>0</sub>-to-TE<sub>1</sub> conversion efficiency over 40 nm bandwidth.

In addition to mode order conversion, photonic inverse design by topology optimization has been widely implemented over several applications, including MDM MUX/DEMUX, polarization beam splitter (PBS), polarization converter and MUX/DEMUX for coarse wavelength division multiplexing (CWDM). For broadband operation, the device should be designed like colorless dielectric meta-material by avoiding the Bragg reflection zone [3]. The reported TE<sub>0</sub>-to-TE<sub>1</sub> converter by topology optimization [2] is designed in photonic crystal operation regime with a narrow bandgap, which intrinsically limits the operation bandwidth. Here we present a family of ultra-compact (~ 4 μm length) devices with inverse design for broadband mode order conversion. TE<sub>0</sub>, TE<sub>1</sub> and TE<sub>2</sub> can be mutually converted with around 85% efficiency and below 1% crosstalk. Unlike most published converters that can only handle conversion between TE<sub>0</sub> and high order modes [1], our work allows direct conversion between different high order modes. With no more necessity of using TE<sub>0</sub> as a stepping stone, in principle our design technique can be applied to arbitrary mode order conversion. The extreme compactness of optimized converter also allows alternative functionalities (such as bending and crossing) to be realized on a small footprint.

## 2. Inverse design and performance

First, a TE<sub>0</sub>-to-TE<sub>1</sub> converter is optimized on a 3.85 μm × 2.35 μm silicon region, which is discretized into a 15 × 25 pixels (rectangular lattice) binary problem. Each pixel represents a fully etched hole with 50 nm radius at 150 nm lattice constant [3], where “1” means a hole etched and “0” means no hole. 150 nm pitch ( $A$ ) is chosen to ensure Bragg wavelength ( $\lambda_{bragg} = 2 \times n_{eff} \times A$ ) is far from C band and this can be confirmed by following equation, where  $n_{eff}$  is the highest effective index of Si waveguide mode (~3).

$$\frac{1550 \text{ nm}}{A} \gg 2 \times n_{eff} \quad (1)$$

The device is assumed to be covered by SiO<sub>2</sub> top cladding, which allows us to use a vertical symmetry boundary condition in 3D FDTD calculation. Input mode source launches a TE<sub>0</sub> mode over 100 nm bandwidth centered at 1.55 μm while transmission and reflection into TE<sub>0</sub> and TE<sub>1</sub> are separately measured by eigenmode expansion

monitors. Here we follow the neural network (NN) assisted direct binary search (DBS) method [4] to conduct optimization with 2000 random training data, which gives faster initial convergence than conventional DBS. After 800 FDTD runs of NN-DBS, conventional DBS [3] is used to refresh the matrix by 3 times for fine optimization. Figure of merit (FOM) is defined as  $TE_1$  power subtracting  $TE_0$  crosstalk and reflection and we attempt to increase FOM during optimization. Lumerical 3D FDTD is used to calculate 11 spectral points from  $1.5 \mu\text{m}$  to  $1.6 \mu\text{m}$ , and the worst spectral value of FOM (worst case scenario) is being tracked and optimized in order to reduce wavelength dependence. During optimization, coarse mesh ( $25 \text{ nm}$ ) is used with vertical symmetry boundary condition to reduce computational time. The finalized structure after optimization is validated under fine mesh ( $5 \text{ nm}$ ) with 51 spectral points over  $100 \text{ nm}$  bandwidth and the perfectly matched layer (PML) condition is used at all boundaries.

Figure 1 shows the finalized geometry after optimization and the major E field component ( $E_y$ ) distribution plot is also shown. From the field distribution, the input beam is split and then merged at the output with the top beam delayed by  $\pi$  phase shift relative to bottom beam. Distributed holes increase the phase velocity of the beam compared with Si region without holes since the average refractive index is reduced. FDTD spectrum shows  $\sim 85\%$  efficiency with  $\sim 0.5\%$  crosstalk and reflection obtained over  $100 \text{ nm}$  bandwidth. Compared with the reported  $TE_0$ -to- $TE_1$  converter based on photonic crystal, the proposed converter works over a substantially broader bandwidth since the device avoids the Bragg reflection zone. The efficiency of the converter can potentially be improved by using a larger matrix, although larger footprint and higher computational effort will be required.

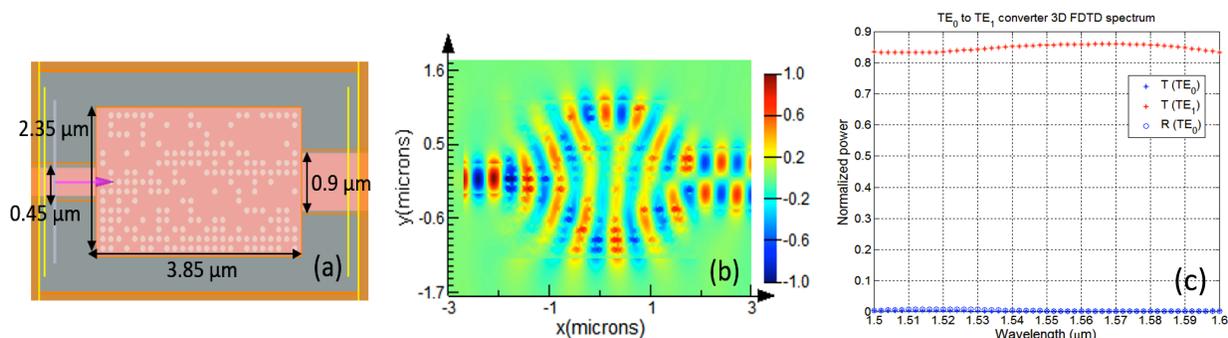


Fig. 1. (a) Optimized geometry, (b)  $E_y$  plot, and (c) 3D FDTD spectrum of the finalized  $TE_0$ -to- $TE_1$  converter

A  $TE_0$ -to- $TE_2$  converter is also designed with a similar procedure. In this case, the two outer lobes of  $TE_2$  should be delayed equally and merged with the center lobe. Therefore, a horizontally symmetric structure ( $20 \times 30$ ) is being evaluated on a  $4.6 \mu\text{m} \times 3.1 \mu\text{m}$  rectangular silicon region. During inverse design, a  $10 \times 30$  matrix (top half of the geometry) is optimized and mirrored to the bottom half of the Si region. Fig.2 (a) shows the finalized geometry after optimization. Field plot shows most majority of input  $TE_0$  splits equally into two outer routes and some fraction of  $TE_0$  is diffracted and refocused at the output waveguide along the middle route. FDTD spectrum of finalized device shows over  $85\%$  efficiency with less than  $1\%$  crosstalk and reflection.  $TE_1$  crosstalk power is almost negligible here because  $TE_0$  input cannot excite  $TE_1$  along a horizontally symmetric structure.

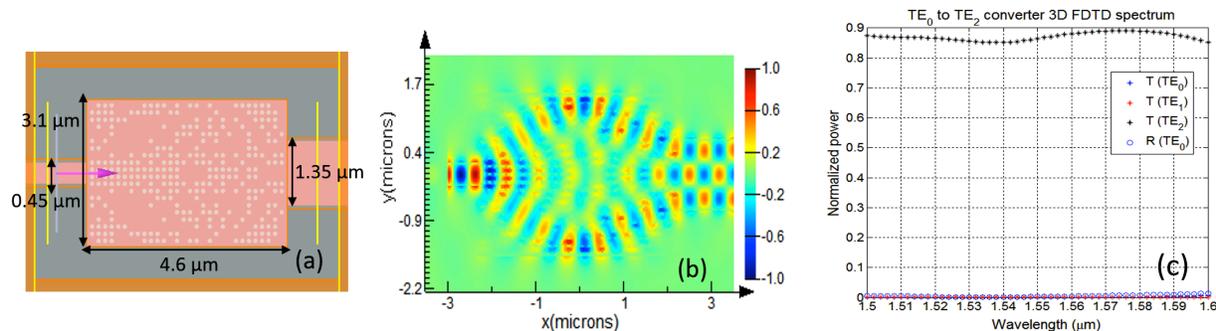


Fig. 2. (a) Optimized geometry, (b)  $E_y$  plot, and (c) 3D FDTD spectrum of finalized  $TE_0$ -to- $TE_2$  converter

A  $TE_1$ -to- $TE_2$  converter is also demonstrated (see fig.3) in the same manner as the  $TE_0$ -to- $TE_1$  converter. The optimized device can obtain roughly  $87\%$  efficiency with crosstalk/reflection into  $TE_0$  and  $TE_1$  both below  $1\%$ . The direct conversion between  $TE_1$  and  $TE_2$  does not demand conversion via  $TE_0$  as a stepping stone. Unlike using a  $60$

$\mu\text{m}$ -long cascaded  $\text{TE}_0$  to high order mode converter based on an adiabatic taper [1], our direct  $\text{TE}_1$ -to- $\text{TE}_2$  converter can achieve 87% efficiency with device length less than  $4 \mu\text{m}$ .

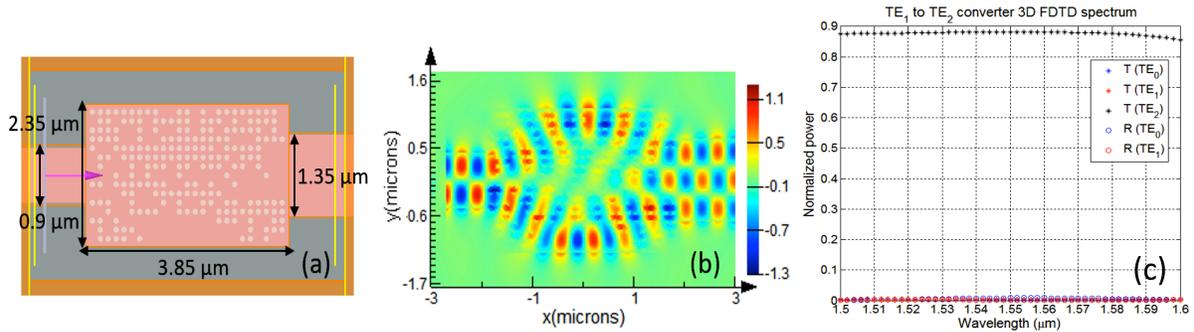


Fig. 3. (a) Optimized geometry, (b) Ey plot, and (c) 3D FDTD spectrum of the finalized  $\text{TE}_1$ -to- $\text{TE}_2$  converter

Our ultra-compact mode order converter can also be cascaded with other devices to process high order modes. As an example, the  $\text{TE}_2$  mode 90-degree cross is demonstrated here, which cascades four  $\text{TE}_0$ -to- $\text{TE}_2$  converters to a conventional  $\text{TE}_0$  90-degree cross [5] at four ports. The total footprint of the  $\text{TE}_2$  90-degree cross is merely  $23 \mu\text{m} \times 23 \mu\text{m}$  and less than 1.5 dB insertion loss can be obtained over 100 nm bandwidth. Only -30 dB  $\text{TE}_0$  crosstalk will be excited at through port over 80 nm bandwidth and all modes excited at cross port are well below -40 dB.

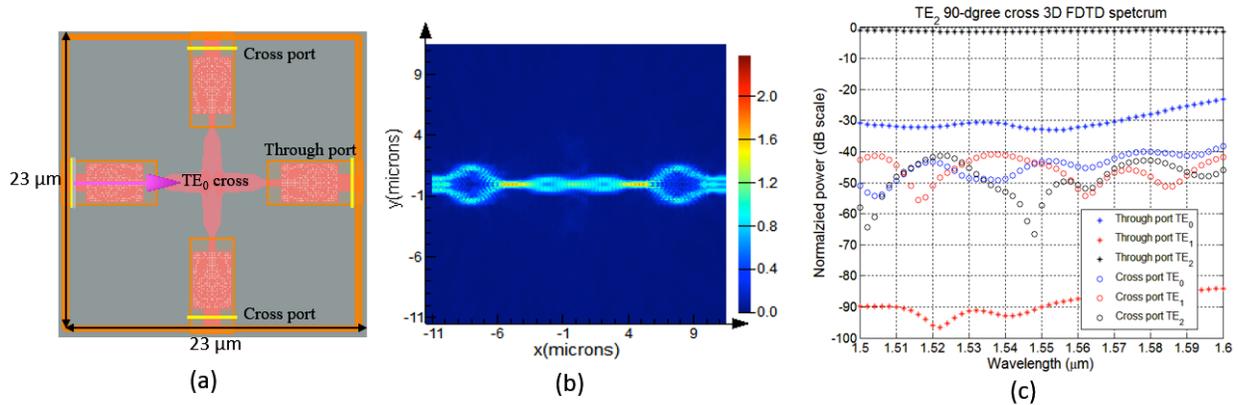


Fig. 4. (a)  $\text{TE}_2$  90-degree cross geometry, (b)  $|E|$  plot, and (c) 3D FDTD spectrum of the  $\text{TE}_2$  90-degree cross

### 3. Conclusion

We numerically demonstrate a family of ultra-compact ( $\sim 4 \mu\text{m}$  length) SOI mode order converters based on a machine-learning-assisted optimization method.  $\text{TE}_0$ ,  $\text{TE}_1$  and  $\text{TE}_2$  can be mutually converted with  $\sim 85\%$  efficiency over 100 nm bandwidth. In principle, our optimization technique can be used to design arbitrary mode order converters. In addition, topology optimized mode order converter can help establishing alternative functionalities (such as crossing and bending) for high order modes with a compact footprint.

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